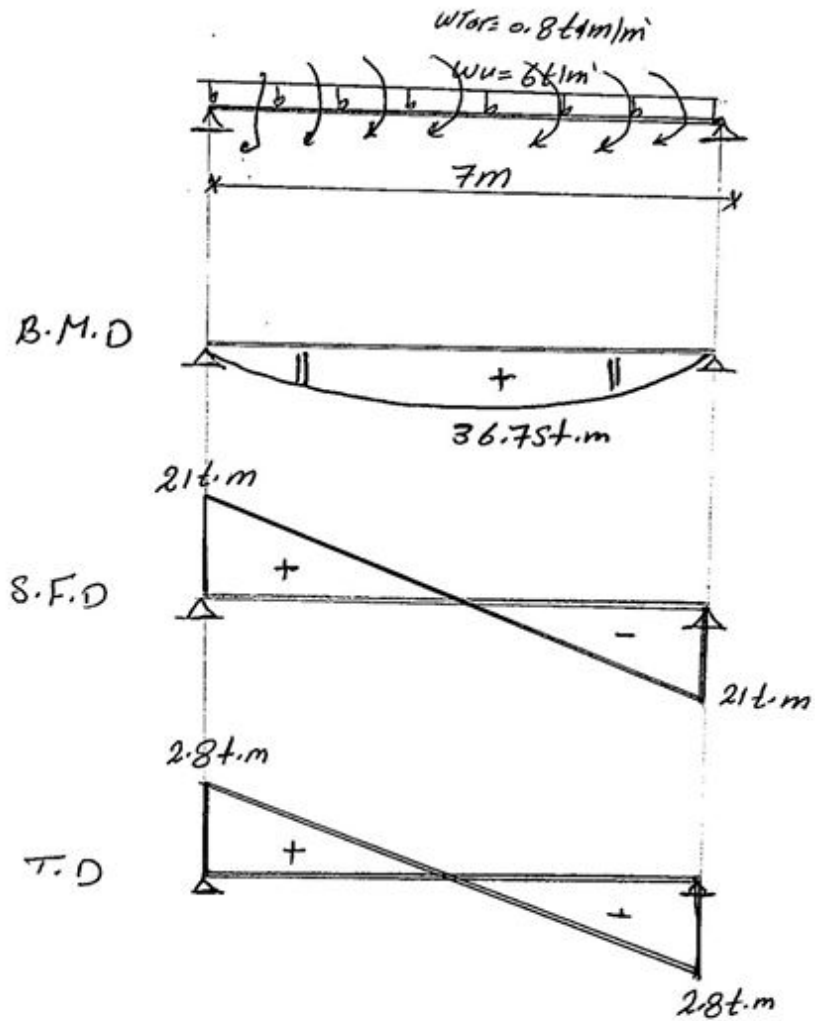


Final exam 2012

قسم الهندسة المدنية

Q1 Design the shown beam due to moment & shear & Torsion.

$$b = 30 \text{ cm}$$



Assum $30 \times 80 \text{ cm}$

① Design beam due to shear & Tor

Shear

$$* q_u = \frac{21 \times 1000}{75 \times 30} = 9.3 \text{ kg/cm}^2$$

$$* S_{si} = \frac{1}{\sqrt{1 + \left(\frac{11.7}{9.3}\right)^2}} = 0.62$$

$$* q_{cu} = 0.62 \times 0.75 \times \sqrt{\frac{f_{cu}}{8}} = 6 \text{ kg/cm}^2$$

$$* q_{max} = 0.62 \times 2.2 \times \sqrt{\frac{250}{1.5}} = 17.6 \text{ kg/cm}^2$$

$$q_{cu} < q_u < q_{max}$$

$$* q_{su} = q_u - \frac{q_{cu}}{2} = 6.3 \text{ kg/cm}^2$$

$$* q_{su} = \frac{n A_{str} f_y / s}{s b}$$

$$6.3 = \frac{2 * A_{str} f_y}{s * 30 * 1.15}$$

$$A_{str} = 1087 \frac{s}{f_y}$$

Torsion

$$q_{tu} = \frac{3 \sqrt{1} t_u}{t b^2} = \frac{3 \times 2.8 \times 10^5}{80 \times 30^2} = 11.7 \text{ kg/cm}^2$$

$$S_{ti} = 0.78$$

$$* q_{cut} = 0.78 \times 0.75 \times \sqrt{\frac{250}{1.5}} = 7.5 \text{ kg/cm}^2$$

$$* q_{nut} = 22.1 \text{ kg/cm}^2$$

$$q_{cu} < q_{ut} < q_{max}$$

$$* q_{sut} = q_u - \frac{q_{cut}}{2} = 11.7 - \frac{7.5}{2} = 8 \text{ kg/cm}^2$$

$$* A_{st} = \frac{S * q_{sut} * b^2 t}{\alpha_c \times \gamma_1 \left(\frac{f_y}{s}\right) * 3}$$

$$* \alpha_c = 25 \text{ cm}$$

$$* \gamma_1 = 70 \text{ cm}$$

$$\alpha_t = 0.66 + 0.33 \times \frac{70}{25} = 1.58 \neq 1.5$$

$$A_{st} = \frac{S \times 8 \times 30^2 \times 80}{1.5 \times 70 \times 25 \times \frac{F_y}{1.15} \times 3}$$

$$A_{st} = 84.11 \frac{S}{F_y}$$

$$\therefore (A_{st} + A_{str}) = 182.8 \frac{S}{F_y}$$

* use #10 $\rightarrow F_y = 3600 \rightarrow (A_{st} + A_{str}) = 0.785$

$$\therefore S = 14.6 \text{ cm} > 10 \text{ cm}$$

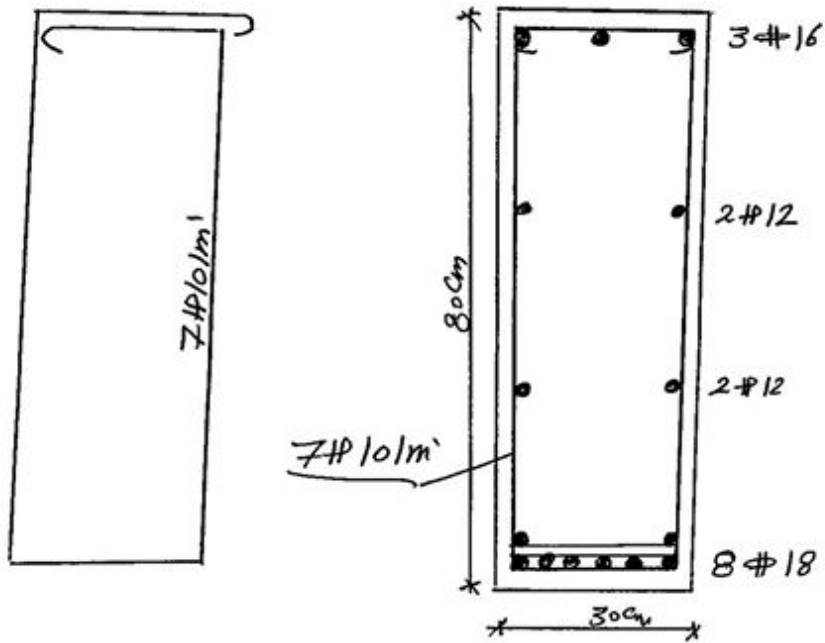
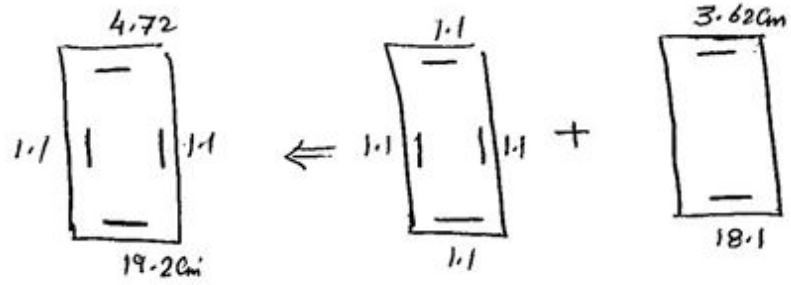
$\therefore N = \frac{100}{S} = 6.8 \rightarrow 7 \#10/m'$
 c/c بتراب \rightarrow main c/c

$$\begin{aligned} * A_{slong} &= \frac{2 A_{st} (x_1 + y_1)}{S'} \left(\frac{P_u}{P_y} \right) \\ &= \frac{2 \times 84.11 (25 + 70)}{3600} = 4.439 \text{ cm}^2 \end{aligned}$$

② Design Moment:-

$$* d = C \sqrt{\frac{36.75 \times 10^3}{250 \times 30}} \rightarrow C = 3.48$$

$$A_s = \frac{36.75 \times 10^3}{3600 \times 0.75 \times 75} = 18.1 \text{ cm}^2$$



② Check deflection:-

1] $M_u = 36.75 \text{ t.m}$

2] $M_{ap} = 24.5 \text{ t.m}$

3] $W_{ap} = 4 \text{ t/m}$

4] $y_t = 40 \text{ cm}$

5] $I_g = \frac{30 \times 80^3}{12} = 1280000 \text{ cm}^4$

6] $F_{ctr} = 0.75 (250)^{2/3} = 29.8 \text{ kg/cm}^2$

7] $E_c = 14000 \sqrt{250} = 221359.4 \text{ kg/cm}^2$

8] $M_{cr} = \frac{F_{ctr} I_g}{y_t} = 9.5 \text{ t.m}$

$M_{ap} > M_{cr}$

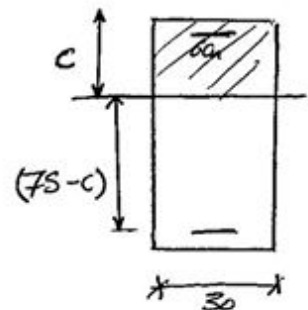
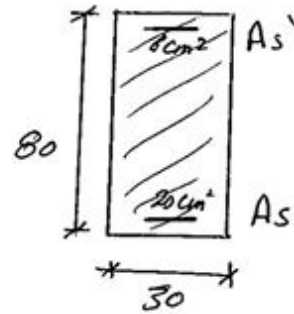
③ Get I_{cr} :-

$$\frac{bc^2}{2} + 15 \times 6 * (c-5) = 15 \times 20 (75-c)$$

$$15c^2 + 90c - 450 = 22500 - 300c$$

$$15c^2 + 390c - 22950 = 0$$

∴ $C = 28.20 \text{ cm}$



$$\begin{aligned} \therefore I_{cr} &= \frac{bc^3}{3} + nA_s' (c-5)^2 + nA_s (d-c)^2 \\ &= \frac{30 \times 28.2^3}{3} + 15 \times 6 \times (28.2-5)^2 + 15 \times 20 \times (75-28.2)^2 \end{aligned}$$

$$I_{cr} = 929771.3 \text{ cm}^4$$

$$\therefore I_e = \left(\frac{M_{cr}}{M_{ap}} \right)^3 I_g + \left[1 - \left(\frac{M_{cr}}{M_{ap}} \right)^3 \right] I_{cr}$$

$$I_e = 950189.8 \text{ cm}^4$$

$$\therefore \Delta I = \frac{5}{384} \frac{WL^4}{E_c I_e}$$

$$= \frac{5 \times 4 \times 10 \times (700)^4}{384 \times 221359.4 \times 950189} = 0.59 \text{ cm}$$

$$\Delta_{act} = 0.59 \text{ cm}$$

$$\Delta_{all} = \frac{L}{250} = \frac{700}{250} = 2.8 \text{ cm}$$

$$\Delta_{act} < \Delta_{all} \rightarrow \text{ok}$$

© Design spiral column to carry $P_u = -500t$

$$\textcircled{1} P_u = 0.4 F_{cu} A_c + 0.67 F_y A_{sc}$$

$$500 \times 10^3 = 0.4 \times 250 \times A_c + 0.67 \times 3600 \times 0.01 A_c$$

$$\therefore A_c = 4028.41 \text{ cm}^2 = \frac{\pi D_c^2}{4}$$

$$D_c = 71.6 \text{ cm}$$

$$\therefore \boxed{D_c = 80 \text{ cm}}$$

$$\boxed{D_k = 75 \text{ cm}}$$

$$\begin{aligned} * A_s &= 0.01 A_c = 50.3 \text{ cm}^2 \\ * A_s &= 0.012 A_k = 53 \text{ cm}^2 \end{aligned} \left. \vphantom{\begin{aligned} * A_s &= 0.01 A_c = 50.3 \text{ cm}^2 \\ * A_s &= 0.012 A_k = 53 \text{ cm}^2 \end{aligned}} \right\} \rightarrow 14 \# 22$$

$$* [V_{sp}]_{min} = 0.36 \left(\frac{F_{cu}}{F_{yp}} \right) \left(\frac{A_c}{A_k} - 1 \right) A_k$$

$$= 0.36 \left(\frac{250}{2400} \right) \left(\frac{80^2}{75^2} - 1 \right) \frac{\pi \times 75^2}{4}$$

$$\boxed{[V_{sp}]_{min} = 22.8 \text{ cm}^2}$$

$$V_{SP} = \frac{\pi A_{SP} D_k}{P} = 22.8$$

$$\frac{\pi * 0.5 * 75}{P} = 22.8 \longrightarrow P = 5.16 \text{ cm}$$

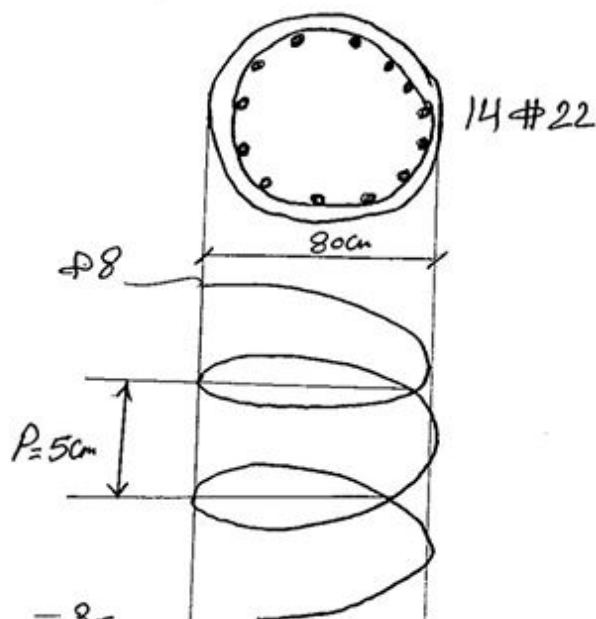
$$\therefore P = 5 \text{ cm} \longrightarrow \phi 8 \text{ حديدية}$$

$$\therefore (V_{SP})_{act} = \frac{\pi * 0.5 * 75}{5} = 23.5 \text{ cm}^2/\text{m}$$

$$\therefore P_u = 0.35 f_{cu} A_k + 0.67 f_y A_{sc} + 1.38 f_{yp} V_{SP}$$

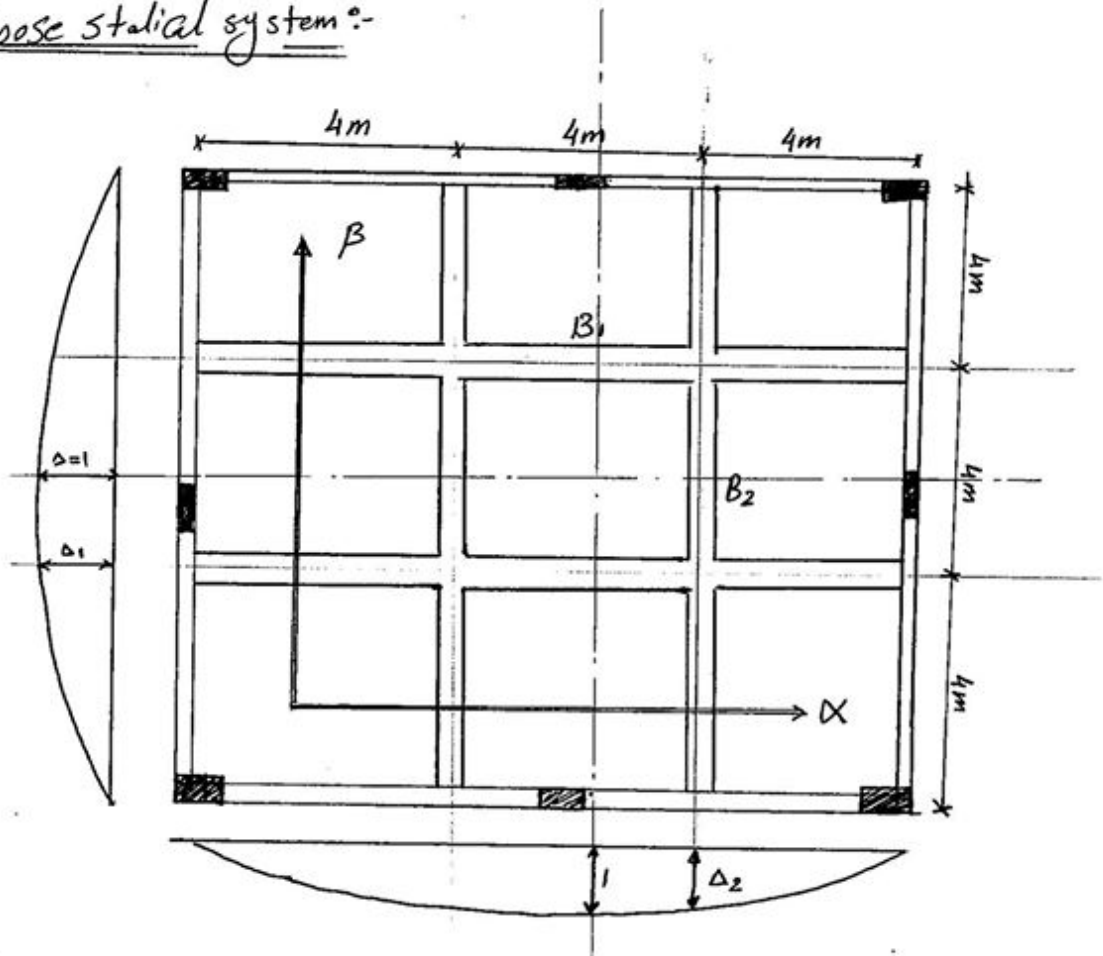
$$= 0.35 \times 250 \times \frac{\pi \times 80^2}{4} + 0.67 \times 3600 \times 14 \times 3.8 + 1.38 \times 2400 \times 23.5$$

$$P_u = 592 \text{ t} > P_{uall} \text{ ok.}$$



Q2 Area $12 \times 12 \text{ m}^2$

① choose statical system:-



② get Conc. Dim:-

$$* t_s = 12 \text{ cm}$$

$$b = 25 \text{ cm}$$

$$t = \frac{L}{14} = \frac{1200}{14} = 85.7 \text{ mm}$$

③ get loads:-

$$* W_{su} = (b_c * t_s + P_c + L.L) * 1.5$$

$$= (0.12 * 25 + 0.15 + 0.4) * 1.5$$

$$W_{su} = 1.28 \text{ t/m}^2$$

$$* O.W_{av} = 0.25 \times (0.8 - 0.12) \times 2.5 \times \frac{4 \times 12}{12 \times 12}$$

$$O.W_{av} = 0.141 \text{ t/m}^2$$

$$\therefore W_{av} = 1.4 \times 0.14 + 1.28$$

$$\therefore W_{av} = 1.48 \text{ t/m}^2$$

4] Design "B₂" \rightarrow at β -dir

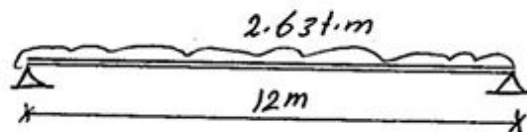
$$* r = \frac{12}{12} \rightarrow 1 \rightarrow \alpha = \beta = 0.5$$

$$* W_u = W_{av} + \phi! \phi * \beta * \Delta$$

$$* \Delta = 1 - \left(\frac{2}{8}\right)^2 = 0.89$$

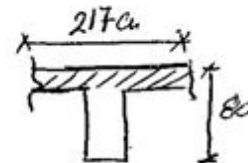
$$* W_u = 1.48 * 4 * 0.5 * 0.89 = 2.63 \text{ t/m}^1$$

$$* M_u = \frac{2.63 \times 12^2}{8} = 47.4 \text{ t.m}$$



$$\left. \begin{array}{l} \text{Bell} \left\{ \begin{array}{l} \rightarrow 16 \times 12 + 25 = 217 \text{ Cm} \\ \rightarrow \frac{12}{8} + 25 = 265 \text{ Cm} \\ \rightarrow 400 \text{ Cm} \end{array} \right\} \rightarrow \text{Bell} = 217 \text{ Cm}$$

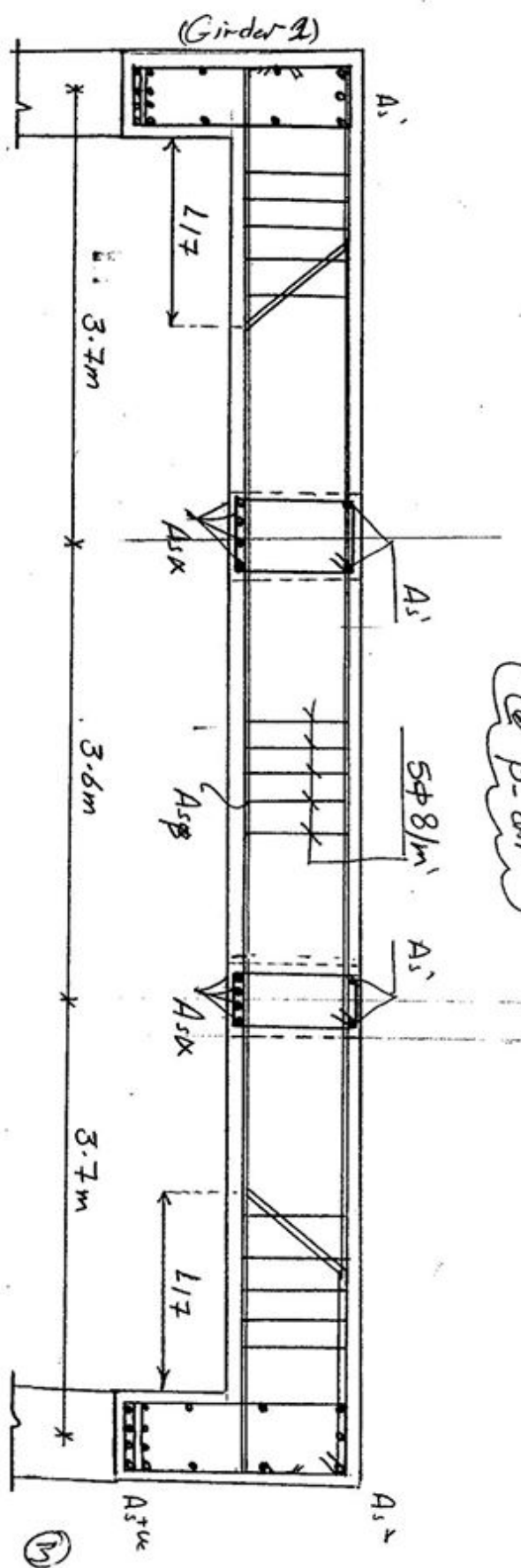
$$* d = G \sqrt{\frac{47.4 \times 10^5}{250 \times 217}} \rightarrow C_1 = 8$$



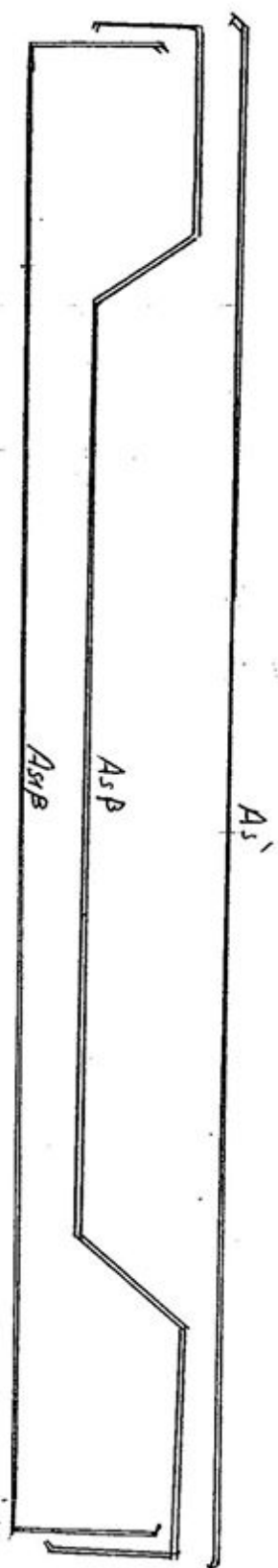
$$d = 80 - 7$$

$$* A_s = \frac{47.4 \times 10^5}{3600 \times 0.826 \times 73} = 21.8 \text{ cm}^2 \rightarrow 9 \# 18$$

B₂
@ B-dr

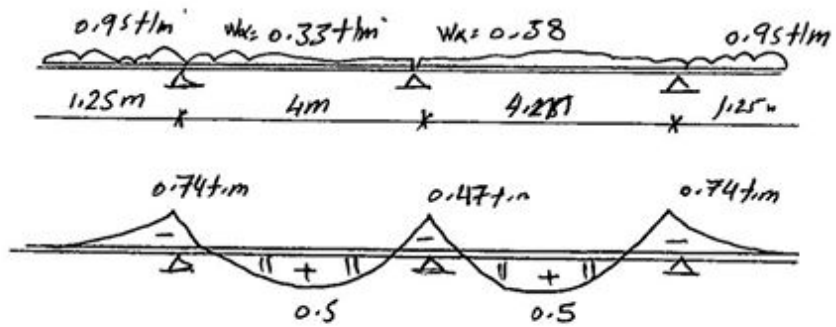


(B)

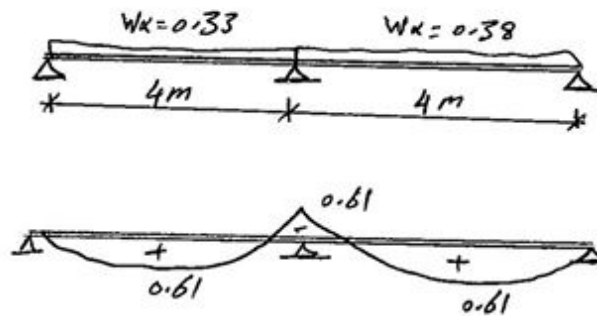


© Take strips:-

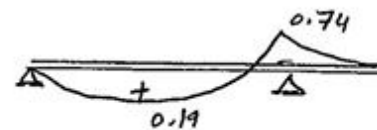
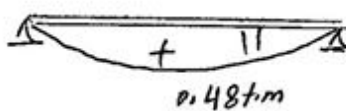
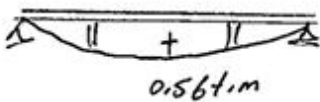
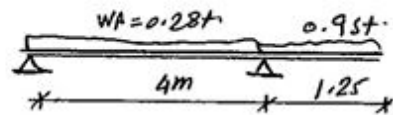
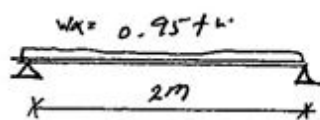
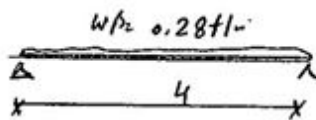
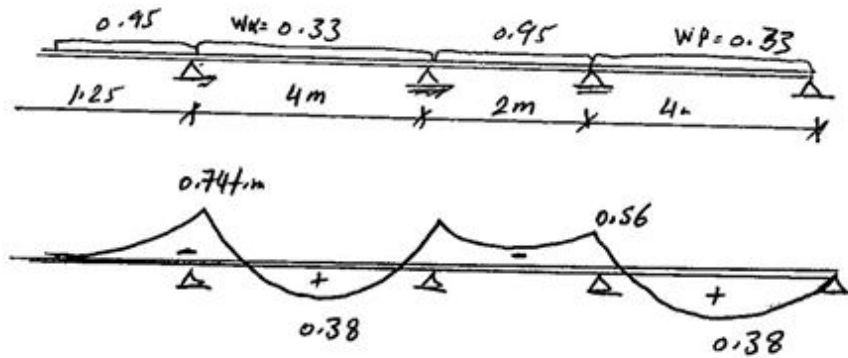
Strip ①



Strip ②



Strip ③



① Design of sec:-

$$* M_{\text{max}}^{+ve} = 0.56 \text{ t.m}$$

$$d = 12 - 2.5 = 9.5 \text{ cm}$$

$$* A_s = \frac{0.56 \times 10^5}{3600 \times 9.5 \times 0.8} = 2 \text{ cm}^2 \rightarrow 5 \# 10 / \text{m}$$

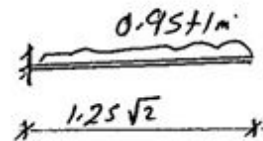
$$* M_{\text{max}}^{+ve} = 0.74 \text{ t.m}$$

$$* A_s = \frac{0.74 \times 10^5}{3600 \times 10.5 \times 0.8} = 2.4 \text{ cm}^2 \rightarrow 5 \# 10 / \text{m}$$

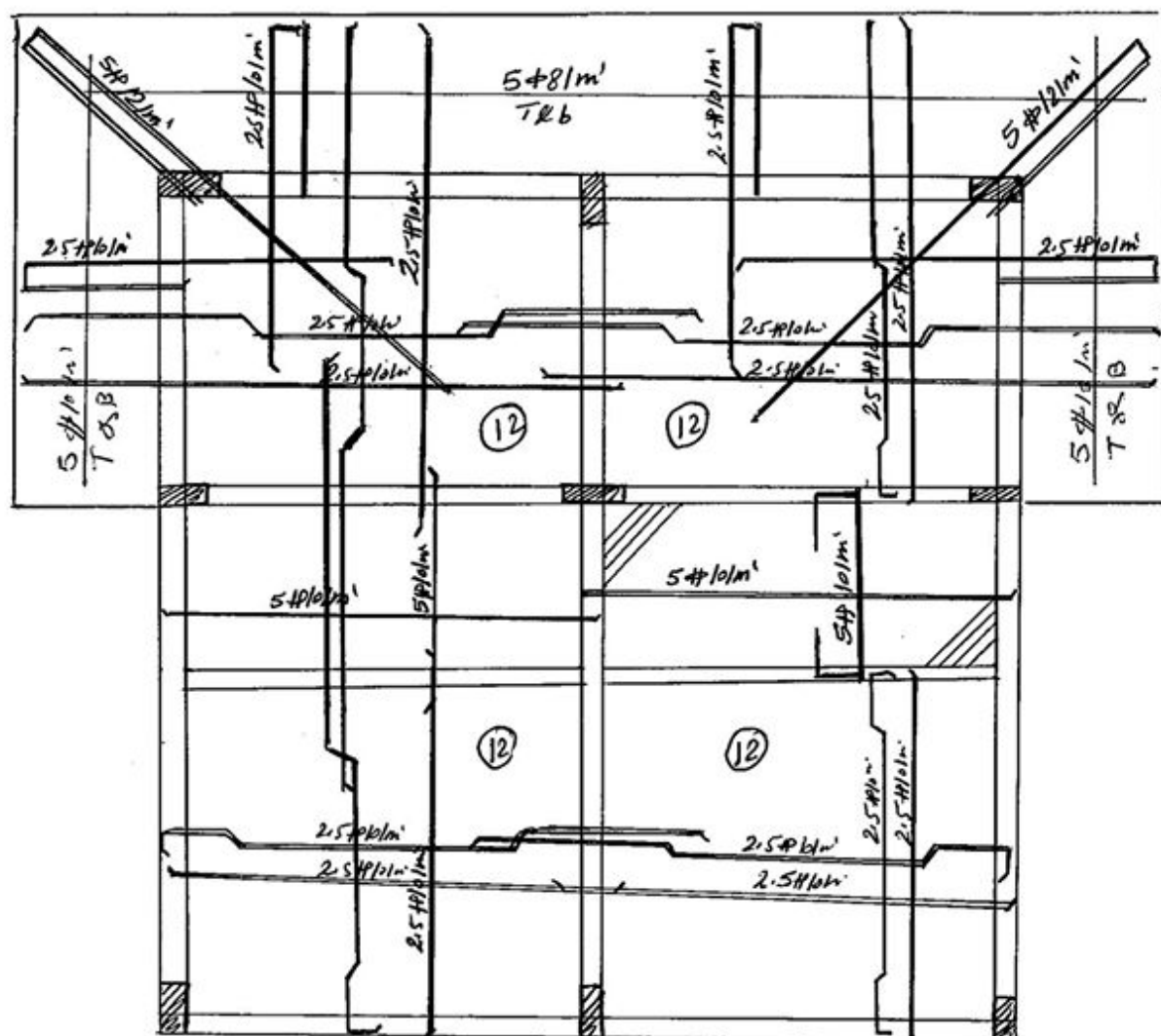
$$* M = \frac{0.95 \times 1.77^2}{2} = 1.48 \text{ t.m}$$

* تصميم الشوكية المرددة

$$* d = G \sqrt{\frac{1.48 \times 10^5}{250 \times 100}} \rightarrow G = \checkmark$$



$$* A_s = \frac{1.48 \times 10^5}{5600 \times 0.8 \times 10.5} = 4.89 \text{ cm}^2 \rightarrow 5 \# 12 / \text{m}$$



24 ① Column "C1"

Col. No	Pu	Lx	Ly	Mx	My	
C1	198t	70cm	30	2.2	2.2	

$$* P_u = 1.1 \times 6 \times 30 = 198 \text{ t}$$

$$* P_u = 111.62 A_c \longrightarrow A_c = 1773 \text{ cm}^2 \longrightarrow L_x = 59$$

$$* M_x = M_y = \frac{WL^2}{36} = \frac{5 \times 4^2}{36} = 2.2 \text{ t.m}$$

① Check buckling:-

x-dir

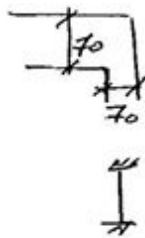
$$* \lambda_x = \frac{3.5 \times 1.2}{0.7} = 6$$

$$\lambda_x < 10$$

short

$$* M_{addx} = 0$$

$$* M_y = 2.2 \text{ t.m}$$



y-dir

$$* \lambda_y = \frac{3.5 \times 1.2}{0.3} = 14$$

$$\lambda_y > 10$$

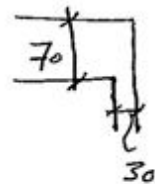
long

$$* M_{addy} = S_y \cdot P_u$$

$$* S_y = \frac{14^2 \times 0.3}{2000} = 0.0294 \text{ m}$$

$$* M_{addy} = 5.82 \text{ t.m}$$

$$M_x = 5.82 + 2.2 = 8 \text{ t.m}$$



$$* e_{min x} = 20 \text{ cm} \quad \left. \begin{array}{l} 0.05 \times 0.7 \end{array} \right\} 0.035 \text{ m}$$

$$* M_{ymin} = 6.93 \text{ t.m}$$

$$M_y = 6.93 \text{ t.m}$$

$$e_{miny} = 20 \text{ cm} \quad \left. \begin{array}{l} 0.05 \times 0.3 \end{array} \right\} 20 \text{ cm}$$

$$(M_x)_{min} = 0.02 \times 198$$

=

$$M_x = 3.96 \text{ t.m}$$

$$\therefore M \rightarrow \frac{6.93}{0.65} = 9.9 < \frac{8}{0.25} = 26.7$$

$$\therefore M_x = 8 + \frac{6.93 \times 0.25}{0.65} \times 0.7 = 9.9 \text{ t.m}$$

$$* e = \frac{9.9}{198} = 0.05 > 0.05 \times 30 = 0.015$$

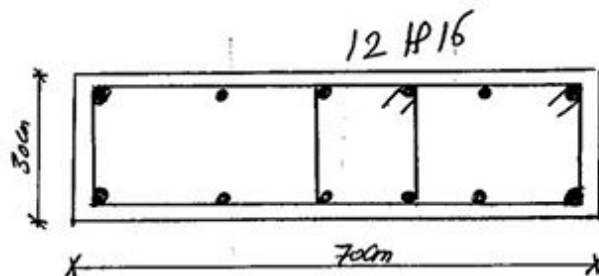
$$* P_b = 102.7 \text{ t} \quad \not\sim P_u \rightarrow \text{Comp. Petite}$$

$$* \frac{P_u}{F_u A_c} = 0.38$$

$$\frac{M_u}{F_u L_x L_y^2} = 0.063$$

$$\rho = 5$$

$$A_s = 5 \times 250 \times 10^{-5} \times 25 \times 70 = 21.9 \text{ cm}^2$$



C₂ Column

GL.No	P _u	L _x	L _y	M _x	M _y
C ₂	264	90	30	2.5	2.05

$$* P_u = 1.1 \times 40 \times 6 = 264 \text{ t}$$

$$* P_u = 111.62 A_c \longrightarrow A_c = 2365 \text{ cm}^2 \longrightarrow L_x = 788 \text{ cm}$$

① check buckling:

x-dir

$$* \lambda_x = \frac{K H_R}{L_x}$$

$$= \frac{1.3 \times 3.5}{0.9} = 5 < 10$$

Short

y-dir

$$* \lambda_y = \frac{1.2 \times 3.5}{0.3} = 14 > 10$$

long

$$* \delta_y = \frac{14^2 \times 0.3}{2000} = 0.0294 \text{ m}$$

$$* M_{\text{add}x} = 7.76 \text{ t.m}$$

$$* (e_y)_{\text{min}} = 20 \text{ mm}$$

$$0.05 \times 0.3 \text{ m}$$

$$* (M_{\text{min}})_y = 5.28 \text{ t.m}$$

$$M_x = 7.76 \text{ t.m}$$

$$* e = \frac{7.76}{264} = 0.029$$

>

$$0.05 \times 0.3 = 0.015$$

$$* P_u > P_b$$

$$* \frac{P_u}{A_c f_u} = 0.39$$

$$\frac{M_u}{250 \times 30^2 \times 90} = 0.038$$

$$S = 4$$

$$* A_s = 4 \times 10^{-5} \times 250 \times 30 \times 90 = 27 \text{ cm}^2$$

14 #16

